

()
INTERSTATE COUNCIL FOR STANDARDIZATION, METROLOGY AND CERTIFICATION
(ISC)

33355
2015
(ISO 7783:2011)

(ISO 7783:2011, MOD)

1.0—92 «
 1.2—2009 «
 1 195 «
 5 «
 2 195 «
 3 18 2015 . 47) (

(3166) 004-97	(3166)004-97	
	AM KG 2 RU TJ	

4 2015 . No 871 - 33355—2015 (ISO 7783:2011) 6
 1 2016 .

5 ISO 7783:2011 Paints and varnishes — Determination of water-vapour transmission properties — Cup method (

6.3.2 «
 no ISO 3233.
 29317—92 (3270:1984) «
 (5.6).
 [2]». 35 «Paints and varnishes».
 ().
 (MOD)

“ “ ”, — () -
“ ”. — , -

1	1
2	1
3	1
4	2
5	3
5.1	3
5.2	3
5.3	($\begin{matrix} 4 & 2 & 0_4 \end{matrix}$).....	3
5.4	3
5.5	3
5.6	4
5.7	4
6	4
6.1	4
6.2	4
6.3	5
6.4	5
7	5
8	6
8.1	V.....	6
8.2	V,.....	6
8.3	s*.....	8
8.4	8
9	8
9.1	8
9.2	R.....	8
10	9
	() (7) 8.3 s _d	10
	().....	11
	() V.....	14
	[2].....	15
	15

Paint materials. Determination of water-vapour transmission properties. Cup method

— 2016—03—01

1

680 $l/(m^2 \cdot d)$ (. . .)
 s_d 0,03) ,
« ».

2

8

7 6709—72
9980.2—2014 (ISO 1513:2010, ISO 15528:2013) ,
(01513:2010 « ».
MOD: 15528:2013 MOD)
29317—92 (3270—84)
31993—2013 (ISO 2808:2007)
(2808:2007 MOD)

3

8

3.1

(water-vapour transmission rate) () V:

1

($l/(m^2 \cdot d)$).

2

8 (. 3.3)

20.4.

3.2 through the test piece) G:

() (rate of flow of water-vapour

3.3 diffusion-equivalent air layer thickness) s_d :

(water-vapour

3.4

(water-vapour resistance factor) :

1

2

3.5

(test piece):

3.6

(wet-cup method):

(93 % 50 %).

3.7

(dry- method):

(50 % 3 %).

3.8

(test assembly):

()

()

(test area):

4

(. 23 °)

(. 50%).

(), 3 % —

93 % —

(),

()

5

5.1

240 (2).

5.2

1

50

10

(5.5).

(5.3)

(5.4)

10 30

5.3

(NH₄H₂PO₄),

(. . .),

6709.

93 %.

8

50 %.

1207

(23 °)

(101325).

5.4

8

4

200

1.6

3 %.

(23 *)

(101325).

50 %.

1400

5.5

5.6

(50 ± 5) %

729317.

0.02 0.3 /

(101325 [1].)

(23 ± 2) °

8.1.

15

5.7 8

50 2

1 ;

10 .

50 2

6

6.1

)

7 9980.2.

() (

—

9980.2.

6.2

6.2.1

50 %

50 %

(23 12) °

6.2.2

7

(5015) %.

/

(23±2)*

7

(5015) %,

(
6.2.3

1 %.

(23 ± 2) °

(50 ± 5) %

28

24

:

- 24 —

• 24 —

(

(50 ± 2) ° .

(2312) ° ;

(23 ± 2) °

(5015) %.

(50 ± 2) °

24

()

(23 ± 2) *

(50 ± 5) %.

24

6.3

d.

31993.

6.4

(5.4) (

10

. 8

10

),

30

(5.3) (

)

50 %.

(. 8.2.1).

7

(5.7)

0.02—0.3 /
(5.6).

()

()

8.2.2

6

G_s

()

$G_{cs} (/) ($

(/)

(/)

G_s

G_s

8.2.3

$$V_{z'} / (\frac{V_{\%}}{2}),$$

$V_{\%} - 24JL. Hi.$

(3)

24 —

$G, / / ;$

—

0 :

G_s —

, —

8.2.4

$$V_{cs'} / (* \frac{V_{cs}}{2}).$$

$$V = 7AJL \text{£}$$

(4)

24 —

$G_{cs} / / :$

—

0 ;

G_{cs} —

% —

8.2.5

$$V / (\frac{V}{2} -).$$

$V,$

V_{ct}

$$! = J \text{---} L$$

$$v, W$$

(5)

$$s \frac{\wedge}{\%} V_{ci}$$

(6)

$$V \quad 680 / (\frac{V}{2}).$$

$$V > 680 / (\frac{V}{2} \cdot) (\cdot \quad 1).$$

f2J

8.3

$$s_d = \frac{v^*}{\dots} \quad (7)$$

$$\frac{v^*}{v} = \frac{0.0169 \sqrt{23^2 + 296^2}}{101325} = \frac{204}{v} \quad (8)$$

$$s_m = 23.7 \quad (9)$$

8.4

$$d = \frac{f \cdot a \cdot i \cdot o}{d} \quad (10)$$

$$s_d = \dots \quad (7)$$

9

9.1

() , 95 % (40 % ())

9.2

R () , R 95 % (100 % ())

10

- a) , : ;
- b) . ;
- c) ; ().
- d) , () .
- e) :
0 (,) ;
) (,) ;
- h) (.2.2,), (;) -
- i) (— 5.2.3) (,) ; () -
- j) ;
- k) , () : s_d V . -
- l) () : (,) -
-) ;
-) ;
-) , ;
-) , ;

()

(7) 8.3

V(), 8.3J

S_d
S_d

8

" 6 **

(.1)

$$s_d = \frac{\delta_a}{\delta_c} d_a$$

(.2)

S_d—
&—
6—
d.—

· I(· ·);
, I(- ·);

(1).

$$\frac{D}{R_v T}$$

(.)

—
R—
t—

(R_y * 0.462 I()):
· [

(. .)

). -296 < 23 *].

D

$$d \left(\frac{\gamma}{T_0} \right)^{1.81}$$

(.4)

0—
.—

10132S
· (273).

0 1.996 2/):

(273

6 7 * 29S

(A.S)

** [o)

$$\frac{1.996 \cdot 2/}{0.462 \cdot 296} I() \cdot \frac{\epsilon > 0 \cdot R}{7} \left(\frac{7}{V81} \right)^v$$

4 $\frac{1996}{0 \cdot 62 \cdot 296} \cdot 1.158 \cdot 0.0169 I()$.

V

$$\frac{V}{\Delta \rho_v} d_a$$

(.6)

V—
—
d—

, r/ 2 :

(.6) (1)
(.2)

$$8 \cdot \frac{4 \Delta p_v}{v}$$

(.7)

0.0169 I(*) 6 296 (.7)

$$8_0 V \frac{0.0169}{v}$$

(.8)

, 1400 .

(.8) s_a · $\frac{23.7}{V}$

, Ap_w, 1207 .

(.8) $\frac{.20}{V}$

()

.1

38 * 90 %- 24 50 2

1 .

a) 60 % , 40 % -

b) 80 % , 50 ° 52 * 20 % ,

c) (); 60 ' 75 ' 1.3 %

, 3 % .

105 ° —110 * -

3 % ,, -

— 1 % .

.2

.2.1

(.2.2).

.2.2

a)

b)

c)

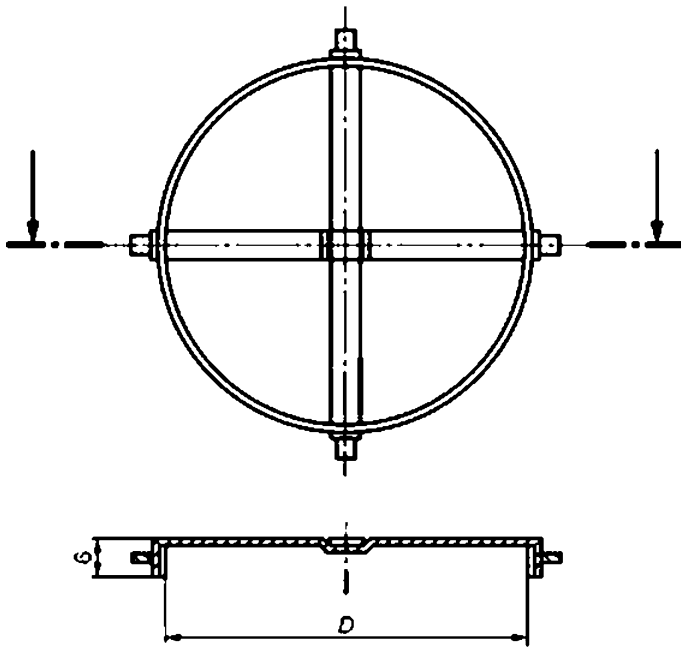
(.1).

45*);

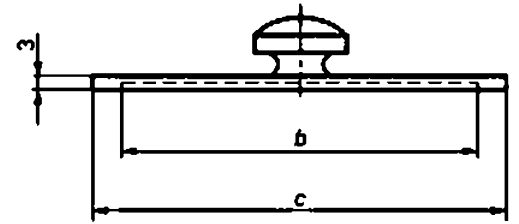
(.1).

(8.1).

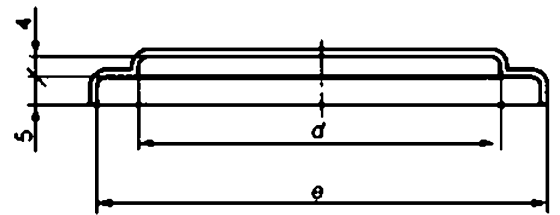
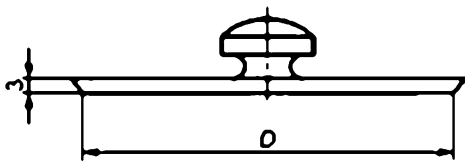
.1



а – Кольцевой трафарет

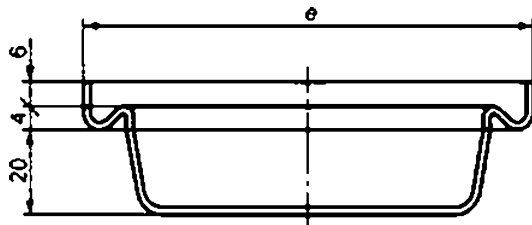


б – Режущий трафарет



d-

(64)



6.1 —

.1—

2					
	<i>D</i>	6		<i>d</i>	
10	35.7	35	45	30	50
15	43.7	45	55	40	60
20	S0.S	50	60	45	65
25	S6.4	S5	65	SO	70
S0	79.8	80	90	75	95
100	112.8	115	125	110	130

.3.1

6.2 6.4

.3.2

(5.3)

(5.4).

10

.3.3

(5.3)

(5.4).

10

1

()

(2)

.1

		2 »)
v_o	—	
v_f		. 150
		. 15 150 .
		15

33355—2015

667.64.001.4:006.354

87.040

MOD

: , ,

. .
. .
. .
. .

16.09.2015. 01.10.2015. 60*64^ .
. . .2.32. - . .1.70. 36 .3164.
« » . 12399S < > . | >..4.
wwM.90sbnlo.ru info^QOSinforu